# Research on the Axial Magnetic Levitation Force Acting on the Ring Magnet Suspended in Magnetic Fluid: Considering a Radial Eccentricity

Jun Yu<sup>1,2\*</sup>, Decai Li<sup>1,3\*</sup>, Nannan Di<sup>1,2</sup>, and Ningning Guo<sup>4</sup>

<sup>1</sup>School of Mechanical, Electronic and Control Engineering, Beijing Jiaotong University, Beijing 100044, China

<sup>2</sup>Key Laboratory of Vehicle Advanced Manufacturing, Measuring and Control Technology (Beijing Jiaotong University),

<sup>3</sup>State Key Laboratory of Tribology, Tsinghua University, Beijing 100084, China

<sup>4</sup>School of Mechanical and Material Engineering, North China University of Technology, Beijing 100144, China

(Received 11 July 2018, Received in final form 12 April 2019, Accepted 12 April 2019)

The self-suspension of magnet in magnetic fluid has been widely used in micromechanical systems, sensors, and dampers. The magnetic field associated with the ring magnet is obtained by numerical calculation and simulation through which the axial magnetic levitation force is calculated, and the numerical calculation, simulation, and experimental results agree with each other. The influence of the radial eccentricity of the ring magnet on the axial magnetic levitation force is studied, the ring magnet will experience a maximum axial magnetic levitation force without radial eccentricity. With the increase of radial eccentricity and the decrease of the distance between the bottom of the ring magnet and container, the axial magnetic levitation force will continue to decrease. But it is noting that the magnitude of the change caused by radial eccentricity is negligible compared to that of the axial magnetic levitation force.

Keywords : magnetic fluid levitation force, self-suspension buoyancy, ring permanent magnet, radial eccentricity

# 1. Introduction

The ferrofluid or magnetic fluid, a new type of functional material with fluidity and magnetism, was synthesized successfully by National Aeronautics and Space Administration to control fluid fuel in a weightless environment for the first time in 1963. It is composed of nanometer magnetic particles (usually Fe<sub>3</sub>O<sub>4</sub>) with a typical diameter of 10 nm, surfactant, and liquid-carrier. The nanometer magnetic particles, coated by the surfactant, are uniformly distributed in the liquid-carrier forming a stable colloid solution. The magnetic fluid will flow to and maintain at the place where the magnetic field is stronger, thus we can control the magnetic fluid by magnetic field.

The combination of magnetism and fluidity makes it possible for magnetic fluid to suspend stably an object whose density is greater than that of magnetic fluid, and this particular phenomenon was discovered by Rosensweig

©The Korean Magnetics Society. All rights reserved.

\*Corresponding author: Tel: +86 13810204816

Fax: +86-10-51684006, e-mail: dcli@bjtu.edu.cn, 16116356@bjtu.edu.cn

for the first time in 1966 [1, 2]. Later in the book titled *"ferrohydrodynamic*", Rosensweig gave a detailed description on the particular magnetic levitation force (self-suspension buoyancy) by means of magnetic fluid stress tensor [3]. Up to now, this property of magnetic fluid has been exploited in many innovative devices, such as dampers [4-6], sensors [7-11], actuators [12-14], bearings [15, 16], micromechanical system [17-19] and so on.

For the typical application of the self-levitation of permanent magnet in magnetic fluid, for example, magnetic fluid sensor [20, 21], damper [22, 23] or energy harvester [24] the diagram of which is shown in Fig. 1. The permanent magnet levitates itself in magnetic fluid contained in a cylindrical container under the magnetic field created by the permanent magnet itself. The permanent magnet is finely balanced in the container radially and damped by the magnetic fluid from radial and axial movements. With axial and radial acceleration (or vibration), the permanent magnet deviates from the center both in radial and axial direction. Axial accelerations tend to produce an axial movement (change of D as shown in Fig. 1) of the magnet which is resisted by the axial magnetic levitation force experienced by the magnet. Radial vibration will

Ministry of Education, Beijing 100044, China



**Fig. 1.** The diagram of a ring magnet suspended in a container filled with magnetic fluid: 1-container, 2-magnetic fluid, 3-ring permanent magnet.

give the inertia mass a radial eccentricity (e as shown in Fig. 1).

Since the vast majority of applications utilize the movement of the magnet in axial direction, the axial magnetic levitation force, which determines the axial movement of the magnet is a key factor to design and manufacture magnetic fluid sensor (damper or energy harvester). But for the use of the magnetic fluid sensor in application, the radial eccentricity of the magnet is useless but inevitable. So, there is a necessity to figure out whether the radial eccentricity has an influence on the axial magnetic levitation force experienced by the magnet.

In the previous studies, for example, in [7, 25-29], the magnetic levitation force experienced by a cylindrical magnet in a cylindrical container filled with magnetic fluid was studied without considering the influence of the radial eccentricity on the axial magnetic levitation force. In [22], the radial magnetic levitation force acting on the cylindrical magnet was studied, but the relationship between radial eccentricity and axial magnetic levitation force was not discussed. The ring magnet has been used in magnetic fluid sensors and dampers as described in [9, 10] and [30], but so far, few articles have studied the magnetic levitation force experienced by a ring magnet self-suspended in magnetic fluid.

In this paper, the axial magnetic levitation force is studied by numerical calculation, magnetic field simulation, and experimental measurement without radial eccentricity at first. Then, the influence of the radial eccentricity of the ring magnet on axial magnetic levitation force is discussed.

# 2. Theoretical Analysis

#### 2.1. Theoretical analysis of magnetic levitation force

According to [3], the equation of motion for magnetic fluid can be expressed as

$$\rho \frac{d\boldsymbol{v}}{dt} = -\nabla p^* + \mu_0 M \nabla H + \rho \boldsymbol{g} + \eta \nabla^2 \boldsymbol{v}$$
(1)

where  $\rho$  is the density of magnetic fluid, v is the velocity of magnetic fluid,  $p^*$  is the composite pressure in magnetic fluid,  $\mu_0$  is the permeability of vacuum, H is the magnitude of magnetic field intensity, M is the magnitude of magnetization of the magnetic fluid, g is the acceleration of gravity, and  $\eta$  is the first coefficient of viscosity of magnetic fluid.

When the ring magnet suspended in a container filled with magnetic fluid as shown in Fig. 1, the magnetic fluid is at rest with v = 0, and equation (1) becomes

$$0 = -\nabla p^* + \mu_0 M \nabla H + \rho g \tag{2}$$

Integrating equation (2) over the volume of magnetic fluid and ignoring the boundary effect which appears at the boundary of the magnetic fluid ( $S_m$  and  $S_c$  as shown in Fig. 1) caused by the different magnetic permeability between magnetic fluid and the magnet, as well as, between magnetic fluid and the container. we have

$$\int_{V_{mf}} (-\nabla p^* + \mu_0 M \nabla H + \rho g) dV = 0$$
(3)

where  $V_{mf}$  is the volume of magnetic fluid, and dV is the infinitesimal volume element.

According to [3],  $p^*$  can be expressed as

$$p^* = p + p_s + p_m \tag{4}$$

where p is the pressure in magnetic fluid in the absence of magnetic field,  $p_s$  is magnetostrictive pressure which can be negligible for an incompressible magnetic fluid, and  $p_m$  is the fluid-magnetic pressure in magnetic fluid which can be expressed as

$$p_m = \mu_0 \int_0^H M dH \tag{5}$$

According to divergence theorem, for  $p^*$ , we have

$$-\int_{V_{mf}} \nabla p^* dV = -\int_{V_{mf}} \nabla p dV - \int_{V_{mf}} \nabla p_m dV = \int_{S_m + S_c} p_m n da + \int_{S_m + S_c} p n da$$
(6)

where da is the infinitesimal area element, n is the unit vector normal to da pointing to magnetic fluid,  $S_m$  is the surface of the magnet, and  $S_c$  is the surface of the container as shown in Fig. 1.

By equation (6), we have

$$-\int_{V_{mf}} \nabla p dV = \int_{S_m + S_c} p n da$$
<sup>(7)</sup>

and

- 248 -

$$-\int_{V_{mf}} \nabla p_m dV = \int_{S_m} p_m n da + \int_{S_c} p_m n da$$
(8)

The magnetic levitation force experienced by the magnet which is the also magnetic force of magnetic fluid on the magnet can be expressed as

$$\boldsymbol{F}_{m} = -\int_{V_{mf}} \nabla p_{m} dV - \int_{S_{m}} p_{m} \boldsymbol{n} da = \int_{S_{c}} p_{m} \boldsymbol{n} da$$
(9)

where n is the unit vector normal to da pointing to the magnetic fluid.

If the permeability of magnetic fluid  $\chi$  is set to be a constant, equation (9) can be rewritten as

$$\boldsymbol{F}_{m} = \frac{1}{2} \oint_{S_{c}} \left( \mu_{0} \int_{0}^{H} \chi H dH \right) \boldsymbol{n} da = \frac{1}{2} \mu_{0} \chi \oint_{S_{c}} H^{2} \boldsymbol{n} da \qquad (10)$$

From equation (10), we can get the magnetic levitation force acting on the magnet as long as the magnetic field strength over  $S_c$  is clear.

#### 2.2. Calculation of the magnetic field strength in magnetic fluid

For a ring magnet with axial uniform magnetization, we can build the physical model using Ampere molecular circulation [31, 32]. The molecular currents cancel out each other inside the ring magnet and over the two end surfaces of the ring magnet, and a net current will appear on the two side surfaces of the ring magnet with the same magnitude but opposite in direction.

For a magnet, we have [33]

$$\frac{|J_0|}{\mu_0} = \frac{J_0}{\mu_0} = i_m \tag{11}$$

where  $J_0$  (or  $B_r$ ) is the remanence vector of the magnet,  $i_m$  is line current density along the shaft of the cylindrical volume (the current per unit length).

To calculate the magnetic field effectively, we establish a cylindrical coordinate system, as well as a cartesian coordinate system, as shown in Fig. 2. The origin of the coordinate is set in the center of one end of the magnet with Z-axis coincides with the axis of the ring magnet.  $P(C, \delta, D)$  is a point outside the ring magnet expressed in cylindrical coordinates,  $r_i$ ,  $r_o$ , and  $l_m$  are the inside radius, outer radius, and axial length of the ring magnet, respectively.

According to the superposition principle of the field, the magnetic induction intensity B at point P must be the vector sum of  $B_o$  (the magnetic induction intensity generated by the magnetizing current over the outer surface of the ring magnet) and  $B_i$  (the magnetic induction intensity



Fig. 2. The cylindrical coordinate and cartesian coordinate system.

created by the magnetizing current over the inner surface of the ring magnet).

The displacement vector from the current element  $i_m$ dzdl over the outer side surface of the ring magnet to the point  $P(C, \delta, D)$  can be expressed as

$$\boldsymbol{R}_{o} = (C\cos\delta - r_{o}\cos\theta)\boldsymbol{e}_{x} + (C\sin\delta - r_{o}\sin\theta)\boldsymbol{e}_{y} + (D-z)\boldsymbol{e}_{z}$$
(12)

where  $e_x$ ,  $e_y$ , and  $e_z$  are the unit vector of X-axis, Y-axis, and Z-axis in cartesian coordinate system, respectively.

The direction of the small current element can be written as

$$d\mathbf{l} = -r_{o}\sin\theta d\theta \mathbf{e}_{x} + r_{o}\cos\theta d\theta \mathbf{e}_{y}$$
(13)

Due to the symmetry of the magnetic induction intensity generated by the ring magnet, the magnitude of magnetic induction *B* must be the same in the place where the coordinate value *C* and *D* are the same in the cylindrical-coordinate system. With  $\delta$  of  $P(C, \delta, D)$ varying from 0 to  $2\pi$ , *B* doesn't change in magnitude. At the point P(C, 0, D), the magnitude of the displacement vector  $\mathbf{R}_o$  can be given as

$$R_{o} = \sqrt{(C - r_{o} \cos \theta)^{2} + (r_{o} \sin \theta)^{2} + (D - z)^{2}}$$
  
=  $\sqrt{C^{2} - 2r_{o}C \cos \theta + (D - z)^{2} + r_{o}^{2}}$  (14)

According to Biot-Savart Law,  $B_o$  at the point P(C, 0, D) can be given as

$$\boldsymbol{B}_{o} = \frac{J_{0}}{4\pi} \int_{-l_{m}}^{0} \int_{0}^{2\pi} \frac{r_{o}(D-z)\cos\theta}{R_{o}^{3}} d\theta dz \boldsymbol{e}_{x} + \frac{J_{0}}{4\pi} \int_{-l_{m}}^{0} \int_{0}^{2\pi} \frac{r_{o}(D-z)\sin\theta}{R_{o}^{3}} d\theta dz \boldsymbol{e}_{y} + \frac{J_{0}}{4\pi} \int_{-l_{m}}^{0} \int_{0}^{2\pi} \frac{(r_{o}^{2} - Cr_{o}\cos\theta)}{R_{o}^{3}} d\theta dz \boldsymbol{e}_{z}$$

$$= B_{ox} \boldsymbol{e}_{x} + B_{oy} \boldsymbol{e}_{y} + B_{oz} \boldsymbol{e}_{z}$$
(15)

where  $B_{ox}$ ,  $B_{oy}$ , and  $B_{oz}$  are the components of the mag-

netic field intensity  $B_o$  at X, Y, and Z-axes in Descartes coordinate system, respectively.

Similarly,  $\boldsymbol{B}_i$  be expressed as

$$\boldsymbol{B}_{i} = B_{ix}\boldsymbol{e}_{x} + B_{iy}\boldsymbol{e}_{y} + B_{iz}\boldsymbol{e}_{z} \tag{16}$$

Thus, we get the magnitude of magnetic field intensity generated by the ring magnet as

$$B = \sqrt{(B_{ox} - B_{ix})^2 + (B_{oy} - B_{iy})^2 + (B_{oz} - B_{iz})^2}$$
(17)

# 3. Numerical Calculation, Simulation, and Experiment

For the typical magnetic fluid inertia sensor, a cylindrical container is used as shown in Fig. 3. We will first do the calculation and simulation with the assumption that the axis of the ring magnet and the container are overlapped, and then the effect of radial eccentricity on axial magnetic levitation force will be discussed.

 $l_c = 45$  mm and  $r_c = 15$  mm are the length and radius of the cylindrical container, respectively.  $l_m = 15$  mm,  $r_i = 3$ mm and  $r_o = 7.5$  mm, and the susceptibility of magnetic fluid used in calculation and simulation is  $\chi = 0.36$ . *D* is the axial distance between the bottom of the container and magnet in range of 0-15 mm, when D = 15 mm, the ring magnet is in the center of the container. *C* is the radial distance from the point P to the axis of the container.

For the cylindrical container used in this paper, the inner surface  $S_c$  can be expressed as

$$S_c = S_{cb} + S_{cs} + S_{ct} \tag{18}$$

where  $S_{cb}$ ,  $S_{cs}$  and  $S_{ct}$  are the bottom, side, and top surface of the cylindrical container, respectively. Due to the symmetry of the magnetic field, the integral of  $p_m$  over  $S_{cs}$ must be zero, and equation (10) can also be written as









Fig. 3. A ring magnet suspended in a cylindrical container.

#### 3.1. Numerical calculation

According to (15)-(17), we can get the magnitude of magnetic induction intensity *B* by MATLAB with just tens of lines of codes. The ring permanent magnet works on its demagnetization curve, the actual remanence is less than the theoretical one, and we set the actual remanence  $J_0 = 1.05T$  (The magnet is made of NdFeB, and the grade of the ring magnet is N35). Suppose that the region of the magnetic fluid is infinite with no flux refraction effect as shown in Fig. 4(a), and the magnitude of magnetic field intensity is

$$H = \frac{B(1+\chi)}{\mu_0(1+\chi)} = \frac{B}{\mu_0}$$
(20)

Let *D* remain the same for the time being with *C* varies within the range of 0-10 mm, we can get *H* over the plane whose axial distance is *D* from the bottom of the magnet (or *H* over  $S_{cb}$ ). Then change the value of *D*, and the magnitude of magnetic field intensity is shown in Fig. 4(b). Based on the magnetic field described in Fig. 4(b), the numerical calculation results of axial magnetic levitation force are presented in Fig. 4(c).



**Fig. 4.** (Color online) (a) Numerical calculation model of magnetic field. (b) The magnetic field over the bottom of the container got by numerical calculation. (c) Numerical calculation results of the axial magnetic levitation force.



**Fig. 5.** (Color online) (a) The physical model of magnetic field simulation; (b) The magnetic field over the bottom of the container got by magnetic field simulation; (c) The simulation results of axial magnetic levitation force.

In addition to numerical calculation, the magnetic field intensity over  $S_{cb}$  and  $S_{ct}$  can also be got by magnetic field simulation using ANSYS. The remanence of the cylindrical magnet is  $B_r = 1.21$ T with the coercivity  $H_c =$ 963000 A/m. The physical model of magnetic field simulation is presented in Fig. 5(a),  $l_d$  is the length of the cylindrical computational domain whose magnitude is 180 mm, and  $r_d$  is the radius of the computational domain, the magnitude of which is 60 mm. The boundary condition of the magnetic field simulation is that the magnetic line is parallel to the boundary of the computational domain. The magnetic field intensity obbtained by simulation is shown in Fig. 5(b) and the simulation results of axial magnetic levitation force are shown in Fig. 5(c).

#### 3.3. Experiment

- 250 -

To measure the axial magnetic levitation force experimentally, a thin, nonmagnetic aluminum rod is attached to



**Fig. 6.** (Color online) (a) Experimental schematic diagram: 1-container, 2-magnetic fluid, 3-ring magnet, 4-nonmagnetic aluminum rod; (b) The experimental results of axial magnetic levitation force.

the top end surface of the magnet. The experimental schematic diagram is shown in Fig. 6(a), the digital Vernier caliper connecting with the dynamometer is installed on the vertical guide screw, which can move up and down when the handle is rotating. The ring magnet is connected with the dynamometer by the thin aluminum rod. The digital Vernier caliper can detect the displacement of the magnet in vertical direction while the dynamometer can measure the axial magnetic levitation force experienced by the ring magnet. The density of the magnetic fluid is 1333 Kg/m<sup>3</sup>. The ring magnet has immersed in magnetic fluid for about 3 days before measurement, and the experimental results are shown in Fig. 6(b).

### 4. Results and Discussion

The numerical calculation, simulation and experimental results are presented in Fig. 7, it is obvious that the numerical calculation, simulation and experimental results



Fig. 7. (Color online) The comparison of numerical calculation, simulation, and experimental results.



Fig. 8. (Color online) (a) The distribution of fluid-magnetic pressure over the bottom of the container; (b) The set coordinate to study the influence of radial eccentricity on axial levitation force.

are in agreement with each other. The axial magnetic levitation force will grow rapidly when the ring magnet moves down.

Now we will discuss the influence of radial eccentricity on the axial magnetic levitation force. According to the distribution of H presented in Fig. 4(b), we can draw the distribution of  $p_m$  over  $S_{cb}$  as shown in Fig. 8(a). We can see from Fig. 8(a) that when the ring magnet gets close to  $S_{cb}$ ,  $p_m$  over  $S_{ct}$  can be ignored. Therefore, equation (19) can also be written as

$$F_m \approx \frac{1}{2} \mu_0 \chi \oint_{S_+} H^2 n da$$
<sup>(21)</sup>

To study the effect of radial eccentricity on the axial levitation force, we set a coordinate system as shown in Fig. 8(b). The origin of coordinate is set at the center of  $S_{cb}$ , and X-axis lies on  $S_{cb}$  with Y-axis normal to  $S_{cb}$ . Y-axis gives the magnitude of  $p_m$  and X-axis gives the radial distance from a point to the origin of the coordinate.

When the symmetry axis of the ring magnet coincides with that of the container, the magnetic field in magnetic fluid is symmetry about the Y-axis, and also  $p_m$  (the solid line denoted by *L* as presented in Fig. 8(b)) is symmetry about the Y-axis. If we rotate the solid line *L* around the Y-axis for 180 degrees, we get a surface which we shall denote by  $V_L$ . The volume enclosed by the surface  $S_L$ ,  $S_{cs}$ , and  $S_{cb}$ , let's denote it by  $V_L$ , equals the magnitude of the axial levitation force acting on the ring magnet.

When the ring magnet deviates from the axis of the container in radial direction, for example, a distance e as shown in Fig. 8(b),  $p_m$  over  $S_{cb}$  will change with the change of the eccentricity e, and also the axial levitation force acting on the magnet. If we ignore the influence of magnetic field refraction effect, the magnetic field generated by the ring magnet will be symmetry about ring

magnet's symmetry axis, as the dotted line L' presented in Fig. 8(b). we rotate the dotted line L' around the symmetry axis of the ring magnet, y', for  $S_L^{180}$  degrees, and get a surface which we shall denote by  $S_L^{-}$ . And the volume enclosed by the surface  $S_L'$ ,  $S_{cs}$ , and  $S_{cb}$ , let's denote it by  $V_{L'}$ , equals the magnitude of the axial levitation force in this case.

According to Fig. 8(b), the magnitude of the enclosed volume should be the maximum when the symmetry axis of the ring magnet coincides with that of the container, and  $\Delta V_L = V_L' - V_L < 0$ . The magnitude of the enclosed volume, which equals the magnitude of the axial magnetic levitation force experienced by the ring magnet will decrease with the emerging of any given radial eccentricity *e*. It is

$$\Delta F_m = F_m' - F_m < 0 \tag{22}$$

With the increase of the radial eccentricity e, the magnitude of the axial magnetic levitation force  $F_m$  will continue to decrease. In this paper, according to the distribution of  $p_m$  presented in Fig. 8(a),  $\Delta F_m$  will be small compared to the magnitude of  $F_m$ . To verify this, we measure  $F_m$  with the same D but different e experimentally. When D = 2 mm with  $F_m = 2.29$ N, the  $\Delta F_m$  corresponding to different eccentricity e is given in

**Table 1.** The relationship between  $\Delta F_m$  and e.

<i>e</i> (mm)	1	2	3	4
$\Delta F_m(\mathbf{N})$	0	-0.01	-0.03	-0.04

**Table 2.** The relationship between  $\Delta F_m$  and e.

	1		
D (mm)	2	4	6
$\Delta F_m(\mathbf{N})$	-0.04	-0.02	0

Table 1.

- 252 -

When D gets smaller,  $p_m$  over  $S_{cb}$  gets larger, and for the same e, the difference between  $V_L'$  and  $V_L$  becomes larger which indicates that the magnitude of  $\Delta F_m$  will increase with the decrease of D for the same e. To verify this, we measure  $F_m$  with the same eccentricity e but different D experimentally. When e = 4 mm, the  $\Delta F_m$ corresponding to different distance D is given in Table 2.

# 5. Conclusion

In this paper, the axial magnetic levitation force experienced by a ring magnet suspended in magnetic fluid is studied and attention is paid to the influence of the ring magnet's radial eccentricity on the axial magnetic levitation force. We obtain the magnetic field in magnetic fluid by numerical calculation and magnetic field simulation based on which the axial magnetic levitation force is calculated. Besides, we measure the magnetic levitation force experimentally, and the experimental results, numerical calculation results, and simulation results agree well with each other. Both theoretical analysis and experimental results show that the ring magnet will experience a maximum axial magnetic levitation force without radial eccentricity, the axial magnetic levitation force will decrease with the emerging of radial eccentricity. With the increase of radial eccentricity and the decrease of the distance between the bottom of the ring magnet and container, the axial magnetic levitation force will continue to decrease, but the magnitude of the change is negligible compared to that of the axial magnetic levitation force. In the research following this paper, we can fill the hole of ring magnet with something, for example, a ferromagnetic material, through which we can expect a change of magnetic levitation force acting on the ring magnet.

## Acknowledgement

This work was supported by "the Fundamenal Research Funds for the Central Universities" (Grant No. 2018YJS145) and "National Defense Science and Technology Innovation Special Zone Project" (Grant No. 18-163-21-TS-001-007-01).

#### References

- [1] R. E. Rosensweig, AIAA J. 4, 10 (1966).
- [2] R E Rosensweig, Nature 210, 5036 (1966).
- [3] R. E. Rosensweig, Ferrohydrodynamics (Cambridge University, New York, 1997) pp 33-73.
- [4] Chuan Huang, Jie Yao, Tianqi Zhang, Yibiao Chen, Huawei Jiang, and Decai Li, J. Magn. 22, 1 (2017).

- [5] X. R. Yang, Q. X. Yang, W. R. Yang, B. Guo, and L. F. Chen, IEEE Trans. Appl. Supercond. 28, 3 (2018).
- [6] Jinghui Peng, Songjing Li, and Hasiaoqier Han, Appl. Phys. Lett. 104, 17 (2014).
- [7] Jun Yu, Xinzhi He, Decai Li, and Wenyi Li, IEEE Sens. J. 18, 6 (2018).
- [8] R. Olaru and D. D. Dragoi, Sensors and Actuators a-Physical 120, 2 (2005).
- [9] D. Y. Lagutkina and M. S. Saikin, J. Magn. Magn. Mater. 431, (2017). DOI: 10.1016/j.jmmm.2016.11.040
- [10] Jie Yao, Yibiao Chen, Zhenkun Li, Tianqi Zhang, and Decai Li, Smart Materials and Structures **25**, 9 (2016).
- [11] L. P. Qian, D. C. Li, and J. Yu, IEEE Sens. J. 16, 23 (2016).
- [12] R. Olaru, A. Arcire, C. Petrescu, and M. M. Mihai, Ieej Trans. Elect. Electron. Eng. 12, 1 (2017).
- [13] Shuai Wu, Chunfang Li, Xiangyu Zhao, and Zongxia Jiao, Appl. Phys. Lett. 111, 21 (2017).
- [14] Babak Assadsangabi, Min Hian Tee, and Kenichi Takahata, J. Microelectromechanical Systems 23, 5 (2014).
- [15] S. G. E. Lampaert, J. W. Spronck, and R. A. J. van Ostayen, Proceedings of the Institution of Mechanical Engineers Part J-Journal of Engineering Tribology 232, 1 (2018).
- [16] Nimeshchandra S. Patel, Dipak Vakharia, and Gunamani Deheri, Industrial Lubrication and Tribology 69, 5 (2017).
- [17] Sayed Mohammad Hashem Jayhooni, Babak Assadsangabi, and Kenichi Takahata, Sensors and Actuators A: Physical 269, (2018). DOI: 10.1016/j.sna.2017.11.020
- [18] Shuai Wu, P. C. K. Luk, Chunfang Li, Xiangyu Zhao, Zongxia Jiao, and Yaoxing Shang, Applied Energy 197, (2017). DOI: 10.1016/j.apenergy.2017.04.006
- [19] Shuai Wu, P. C. K. Luk, Chunfang Li, Xiangyu Zhao, and Zongxia Jiao, IEEE Trans. Magn. 53, 9 (2017).
- [20] L. P. Qian and D. C. Li, Journal of Sensors (2014).
- [21] Leping Qian, Decai Li, and Jun Yu, IEEE Sens. J. 15, 12 (2015).
- [22] W. M. Yang, P. K. Wang, R. C. Hao, and B. H. Ma, J. Magn. Magn. Mater. 426, (2017). DOI: 10.1016/ j.jmmm.2016.11.099
- [23] Wenming Yang, Decai Li, Xinzhi He, and Qiang Li, Int. J. Appl. Electromagnetics Mech. 40, 1 (2012).
- [24] Y. Wang, Q. Zhang, L. Zhao, Y. Tang, A. Shkel, and E. S. Kim, Appl. Phys. Lett. 109, 20 (2016).
- [25] Jun Yu, Jiawei Chen, and Decai Li, J. Magn. Magn. Mater. 469, (2019). DOI: 10.1016/j.jmmm.2018.08.080
- [26] Jun Yu, Du Hao, and Decai Li, J. Phys. D-Appl. Phys. 51, 1 (2018).
- [27] Jun Yu, Xinzhi He, Decai Li, and Wenyi Li, Phys. Fluids 30, 9 (2018).
- [28] Wenming Yang, J. Vib. Control. 23, 14 (2017).
- [29] Xinzhi He Jun Yu, Decai Li and Rongkun Dai, Journal of Beijing Jiaotong University 42, 4 (2018).
- [30] S. Sudo and A. Nakagawa, Int. J. Mod. Phys. B 19, 7

(2005).

- [31] C. Q. Zhang, P. Zhao, F. Gu, J. Xie, N. Xia, Y. He, and J. Z. Fu, Anal. Chem. 90, 15 (2018).
- [32] C. Akyel, S. I. Babic, and M. M. Mahmoudi, Progress in

Electromagnetics Research-Pier **91**, (2009). DOI: 10.2528/ PIER09021907

[33] P. C. Xia, Permanent magnetic mechanism (Beijing University of Technology Press, Beijing, 2000) p 4.