

# Increase in Coercive Field by Magnetoelastic Coupling in Co/VO<sub>2</sub> Films

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Herein, a ferromagnetic cobalt (Co) film was deposited on a VO<sub>2</sub> film exhibiting a structural phase transition from monoclinic to tetragonal at ~340 K to investigate the magnetoelastic effect caused by a phase-transition-induced strain. First, (100) and (101) VO<sub>2</sub> films with thicknesses of 11–43 nm were grown on Al<sub>2</sub>O<sub>3</sub> using pulsed laser deposition, and 2.5-nm-thick Co films were deposited on top of them via sputtering. The magneto-optic Kerr effect hysteresis loops were measured with the temperature variation across the structural phase transition temperature of VO<sub>2</sub>. Upon heating, an increase in the coercive field of the Co layer was observed at the structural phase transition temperature of VO<sub>2</sub>, suggesting a magnetoelastic coupling between the Co and VO<sub>2</sub> layers. The coercive field increment diminished with decreasing VO<sub>2</sub> thickness, and it disappeared as the VO<sub>2</sub> became thinner than a critical value of ~11 nm. These results imply that a phase-transition-induced strain in the VO<sub>2</sub> layer can be used to change the coercive field of the neighboring magnetic layer.

**Keywords :** magnetoelastic coupling, magnetic film, VO<sub>2</sub>, structural phase transition

## 1. Introduction

Magnetic materials can display a change in their magnetic property via deformation (or lattice strain), i.e., the magnetoelastic effect (or inverse magnetostriction). A stress can be directly applied on a material to induce deformation, or it can be delivered to a neighboring material via elastic coupling between the two materials. In magnetic heterostructures, a strain-transfer behavior from a neighboring layer (or a substrate) to a ferromagnetic layer has been used to induce a magnetoelastic effect [1–3]. In particular, ferroelectric or piezoelectric materials were used to generate a controllable strain through an inverse piezoelectric effect [4, 5]. Although a strain of 0.1–0.5 % in piezoelectric materials is not large, the magnetoelastic effect was clearly observed in an epitaxially grown ferroelectric (or piezoelectric)/ferromagnetic bilayer. For example, a ferroelectric BaTiO<sub>3</sub> has a maximum strain of ~0.5 % when it undergoes a rhombohedral-to-orthorhombic transition at ~190 K and an orthorhombic-to-tetragonal transition at ~275 K. Previous works have demonstrated that such structural phase transitions induce a magnetization change in the neighboring magnetic films

[6–8]. Similarly, piezoelectric materials, such as PbZr<sub>x</sub>Ti<sub>1-x</sub>O<sub>3</sub> and Pb(Mg<sub>1/3</sub>Nb<sub>1/3</sub>)<sub>1-x</sub>Ti<sub>x</sub>O<sub>3</sub>, have been used to induce a magnetoelastic effect to the neighboring magnetic layer through an inverse piezoelectric effect controlled by an electric field [9–13].

Vanadium dioxide VO<sub>2</sub> exhibits a structural phase transition from monoclinic to tetragonal at a metal-insulator transition temperature  $T_{MI}$  of 340 K, which is accompanied by a change of ~0.7 % in the  $c$  lattice constant [14]. Polycrystalline or epitaxial VO<sub>2</sub> films can be grown on glass, silicon, sapphire, and TiO<sub>2</sub> substrates for various applications [15–19]. Interestingly, structural-transition-induced strain can modify the magnetization and the coercive field in ferromagnetic Ni or [Co/Pt] films coupled with VO<sub>2</sub> [20–23]. Recently, Venta reported that a Ni film coupled with VO<sub>2</sub> displayed a large coercive field change of 15–50 % at  $T_{MI}$  [21]. In addition, Wei reported that the perpendicular magnetic anisotropy in a [Co/Pt] film coupled with VO<sub>2</sub> disappeared as the temperature exceeded  $T_{MI}$  [23]. These results may be partly caused by the typical decreasing tendency of the magnetic strength of a magnetic material with increasing thermal fluctuation. Nevertheless, these reports suggest that the structural phase transition of VO<sub>2</sub> can generate a distinctive strain in the neighboring layer at the structural phase transition temperature, thus causing a magnetoelastic effect in the neighboring magnetic layer coupled with VO<sub>2</sub>. Similarly,

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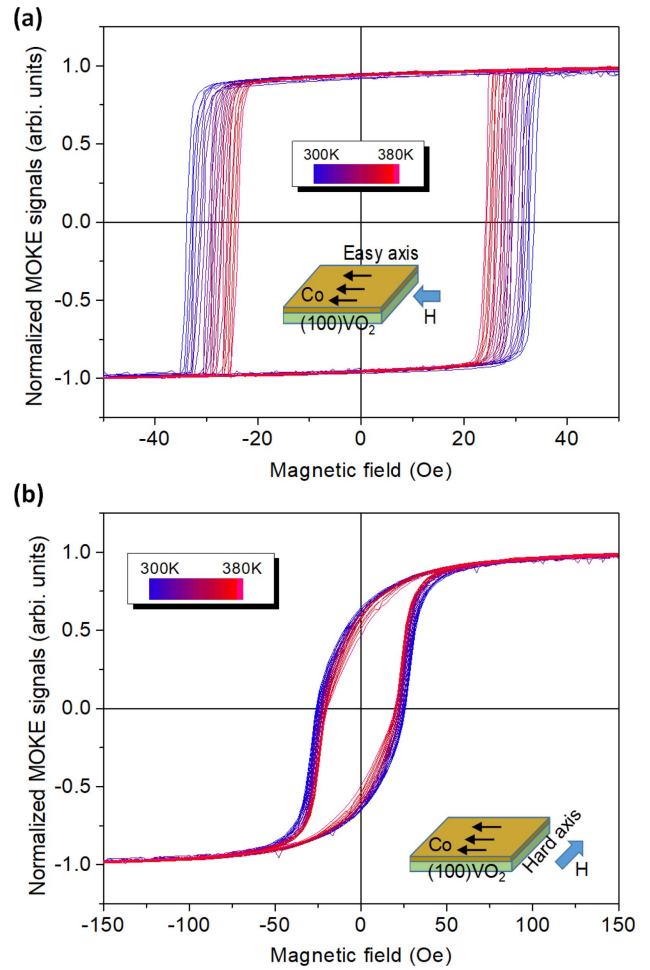
ferromagnetic Ni or Co films on V<sub>2</sub>O<sub>3</sub> exhibited a change in their magnetization and coercivity because of phase-transition-induced strain [21]. The VO<sub>2</sub> thickness dependence of the magnetoelastic effect in ferromagnet/VO<sub>2</sub> systems has not been examined. In the current work, we investigated the temperature dependence of the coercive field of a Co layer coupled with 11-43-nm-thick VO<sub>2</sub> films. The increase in the coercive field of the Co layer at the structural phase transition temperature was attributed to a magnetoelastic effect in the Co layer, which was caused by a phase-transition-induced strain in VO<sub>2</sub>. The increment disappeared when the VO<sub>2</sub> thickness decreased to a critical value of ~11 nm.

## 2. Experiments

Heteroepitaxial VO<sub>2</sub> films were prepared on Al<sub>2</sub>O<sub>3</sub> substrates via pulsed laser deposition. Polycrystalline V<sub>2</sub>O<sub>3</sub> and an Nd:YAG laser with a wavelength of 355 nm and a frequency of 1 Hz were used. During the deposition, the substrate temperature was fixed at 550 °C, and the oxygen partial pressure was maintained at 13 mTorr. Then, (100)- and (101)-oriented VO<sub>2</sub> films were grown on a C-plane Al<sub>2</sub>O<sub>3</sub> and an R-plane Al<sub>2</sub>O<sub>3</sub>, respectively. [17, 18] Next, 2.5-nm-thick Co films were deposited on 43-, 22-, and 11-nm-thick VO<sub>2</sub> films using direct current (dc) sputtering at room temperature. The dc sputtering power was 20 W, and the Ar pressure was 4 mTorr. The root-mean-square roughness of the VO<sub>2</sub> films was about 1 nm. The temperature dependence of the resistance of the VO<sub>2</sub> films was investigated through four-point probe measurement in the temperature range of 290-380 K. The magnetic property of the Co layer coupled with VO<sub>2</sub> was investigated by a magneto-optic Kerr effect (MOKE) setup. The temperature dependence of the coercive field was obtained from the normalized MOKE hysteresis loop, which was measured upon heating and cooling.

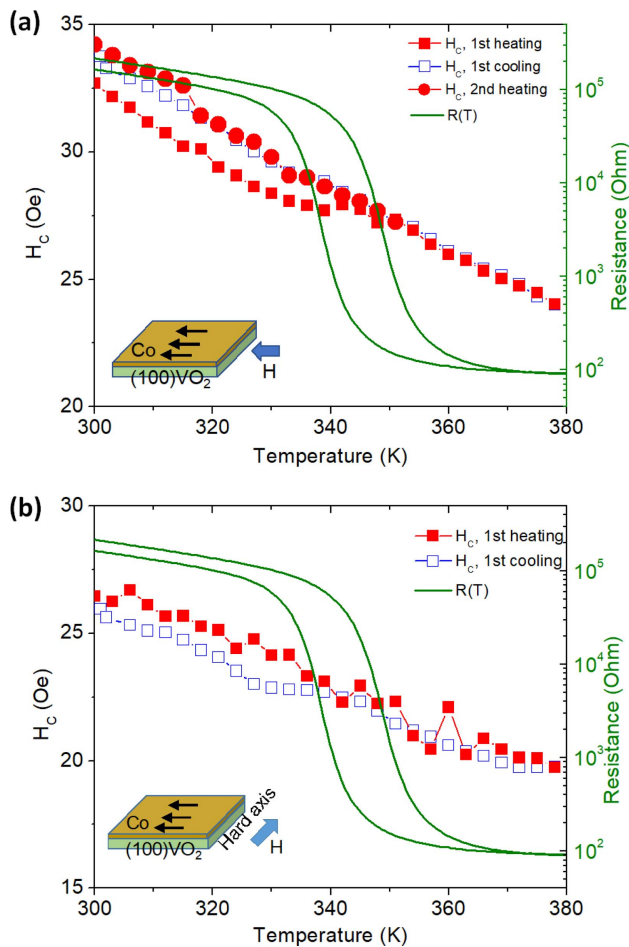
## 3. Results and Discussions

Figure 1 shows the magnetic-field-dependent MOKE signals of the Co film on the 43-nm-thick (100) VO<sub>2</sub>/C-plane Al<sub>2</sub>O<sub>3</sub> at various temperatures from 300 to 380 K. The normalized MOKE signals were measured by applying a magnetic field along the easy-axis and hard-axis directions within the plane. For the easy-axis direction, the MOKE hysteresis loops at room temperature displayed a square-like shape with a saturation behavior of ~35 Oe. The saturation behavior along the hard-axis direction can be observed above ~75 Oe. As the temperature increased, the coercive field ( $H_C$ ) values for both



**Fig. 1.** (Color online) Magnetic field dependence of MOKE signals of Co film deposited on 43-nm-thick (100) VO<sub>2</sub>/C-plane Al<sub>2</sub>O<sub>3</sub> at various temperatures from 300 to 380 K (a) when the magnetic field ( $H$ ) is parallel to an in-plane easy-axis direction and (b) when  $H$  is parallel to an in-plane hard-axis direction.

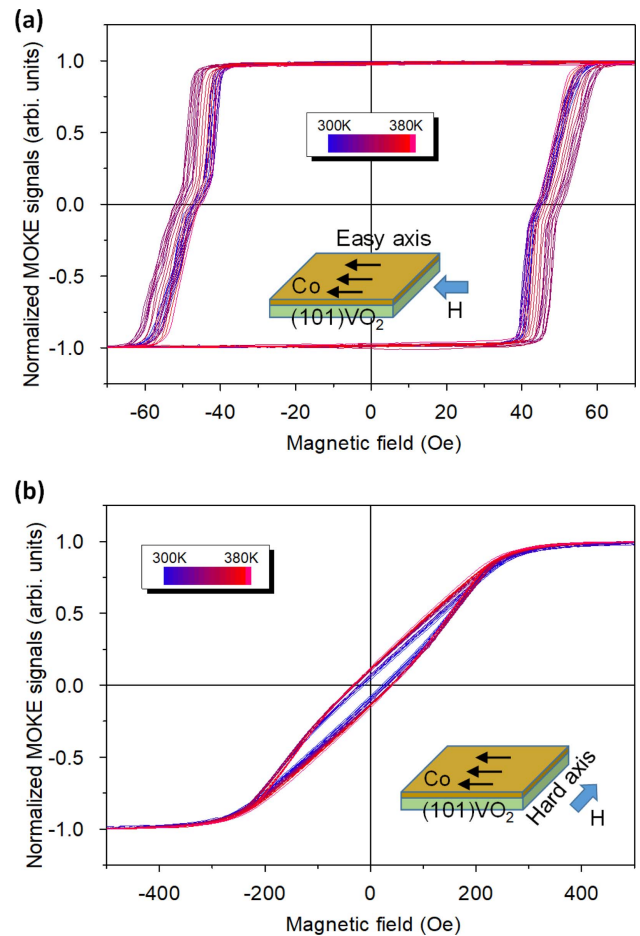
directions monotonously decreased. Figure 2 displays the temperature-dependent coercive field  $H_C(T)$  of the Co film on the (100) VO<sub>2</sub>/C-plane Al<sub>2</sub>O<sub>3</sub> for the easy-axis and hard-axis directions. The  $H_C$  values were obtained with a repetitive temperature change of heating and cooling. The temperature-dependent resistance  $R(T)$  of the (100) VO<sub>2</sub> film on the C-plane Al<sub>2</sub>O<sub>3</sub> substrate upon heating and cooling is also displayed. For the first heating, the  $H_C(T)$  curve along the easy-axis direction exhibited a decreasing tendency with a slight slope change at  $T_{MI}$ . Presumably, the observed change in  $H_C$  at  $T_{MI}$  may be associated with a magnetoelastic coupling between Co and (100) VO<sub>2</sub>, which was caused by the structural phase transition of VO<sub>2</sub> at  $T_{MI}$ . For the subsequent first cooling and second heating treatments, the  $H_C(T)$  curve did not show a clear slope change at  $T_{MI}$ . The change at  $T_{MI}$



**Fig. 2.** (Color online) Temperature versus coercive field  $H_C$  of Co film deposited on 43-nm-thick (100)  $\text{VO}_2/\text{C-plane Al}_2\text{O}_3$  (a) when the magnetic field  $H$  is parallel to an in-plane easy-axis direction and (b) when  $H$  is parallel to an in-plane hard-axis direction. The temperature dependence of the resistance  $R(T)$  of the (100)  $\text{VO}_2$  on the C-plane  $\text{Al}_2\text{O}_3$  is displayed together.

seemingly weakened by an irreversible change in the interface between the Co and (100)  $\text{VO}_2$  after heating up to 380 K. For the hard-axis direction, the  $H_C(T)$  curve exhibited a decreasing tendency without any distinctive change at  $T_{\text{MI}}$ .

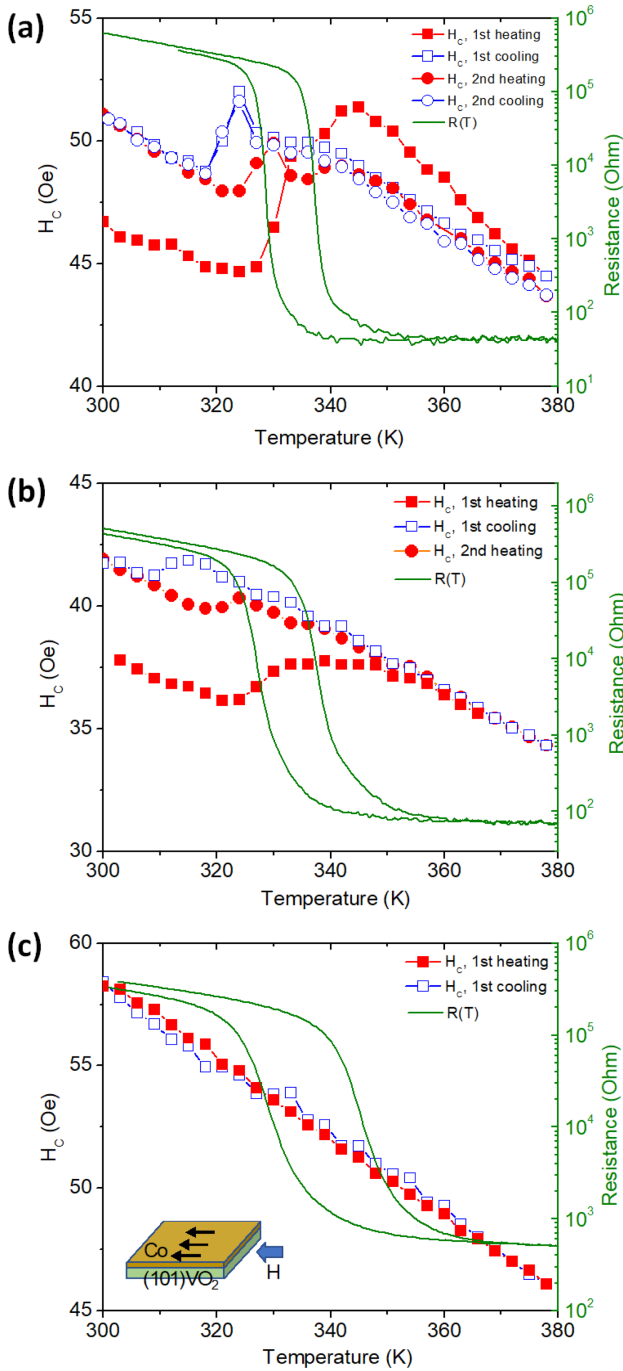
Figure 3 shows the magnetic-field-dependent MOKE signals of the Co film on the 43-nm-thick (101)  $\text{VO}_2/\text{R-plane Al}_2\text{O}_3$  at various temperatures from 300 to 380 K. The normalized MOKE signals were measured by applying a magnetic field along the easy-axis and hard-axis directions within the plane. As the temperature increases, the MOKE hysteresis loops didn't now show a monotonous change but a rather anomalous change in the coercivity  $H_C$ . The (101)-oriented  $\text{VO}_2$  films, with thicknesses of 43, 22, and 11 nm, were used to study the



**Fig. 3.** (Color online) Magnetic field dependence of MOKE signals of Co film deposited on 43-nm-thick (101)  $\text{VO}_2/\text{R-plane Al}_2\text{O}_3$  at various temperatures from 300 to 380 K (a) when the magnetic field ( $H$ ) is parallel to an in-plane easy-axis direction and (b) when  $H$  is parallel to an in-plane hard-axis direction.

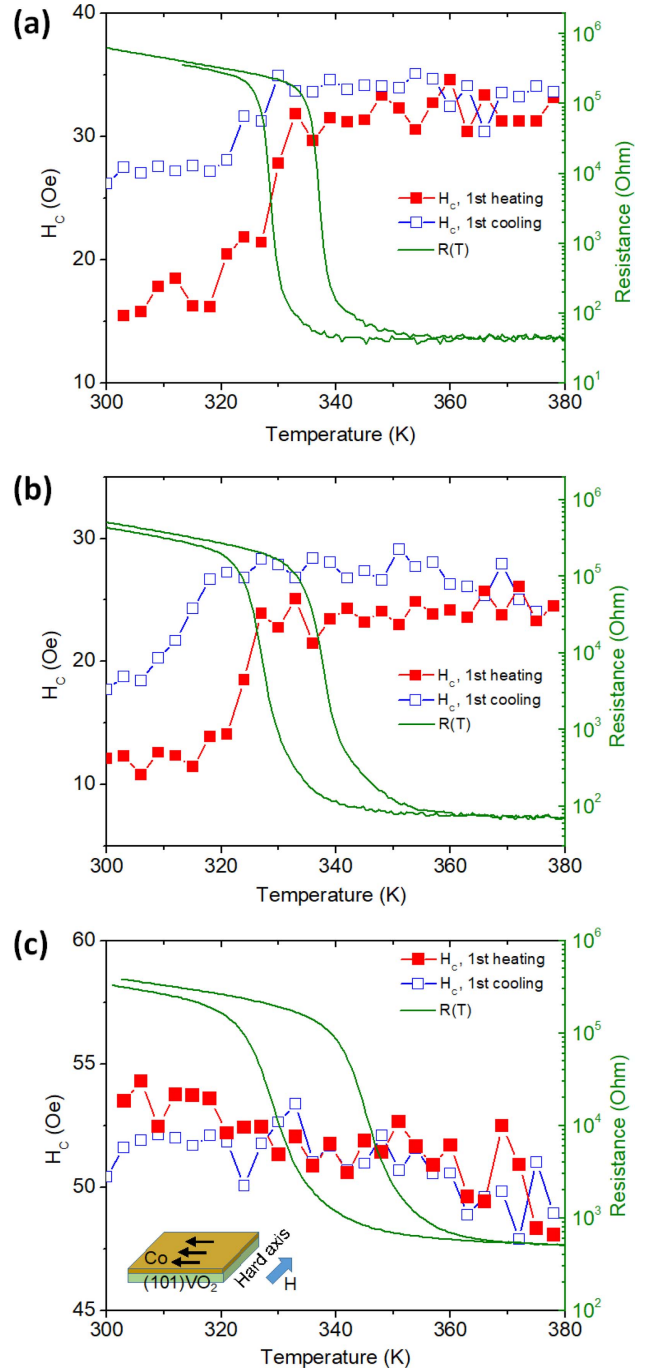
magnetoelastic coupling. Figure 4 displays the temperature-dependent coercivity,  $H_C(T)$ , of the Co film on the (101)  $\text{VO}_2/\text{R-plane Al}_2\text{O}_3$  substrate. As shown in the inset of Figure 4(c), the magnetic field was applied along the easy-axis direction. In all three samples,  $H_C(T)$  commonly exhibited a decreasing tendency with increasing temperature. For the first heating, remarkably, the  $H_C(T)$  of the Co film on the 43-nm-thick (101)  $\text{VO}_2$  displayed a sudden increase from  $\sim 44$  Oe to  $\sim 53$  Oe at  $T_{\text{MI}}$ . Such a change at  $T_{\text{MI}}$  was reduced by the subsequent cooling and heating treatments. In addition, the change in the  $H_C$  value at  $T_{\text{MI}}$  was weakened in the sample with the 22-nm-thick (101)  $\text{VO}_2$ , and it was not observed in the sample with the 11-nm-thick (101)  $\text{VO}_2$ .

Figure 5 displays the temperature-dependent coercivity,  $H_C(T)$ , of the Co film on the (101)  $\text{VO}_2/\text{R-plane Al}_2\text{O}_3$  substrate in the hard-axis direction. The inset of Figure



**Fig. 4.** (Color online) Temperature versus easy-axis coercive field  $H_C$  of Co film deposited on (a) 43-nm-, (b) 22-nm-, and (c) 11-nm-thick (101) VO<sub>2</sub>/R-plane Al<sub>2</sub>O<sub>3</sub>. The temperature dependence of the resistance  $R(T)$  of the (101) VO<sub>2</sub> on the R-plane Al<sub>2</sub>O<sub>3</sub> upon heating and cooling is displayed together.

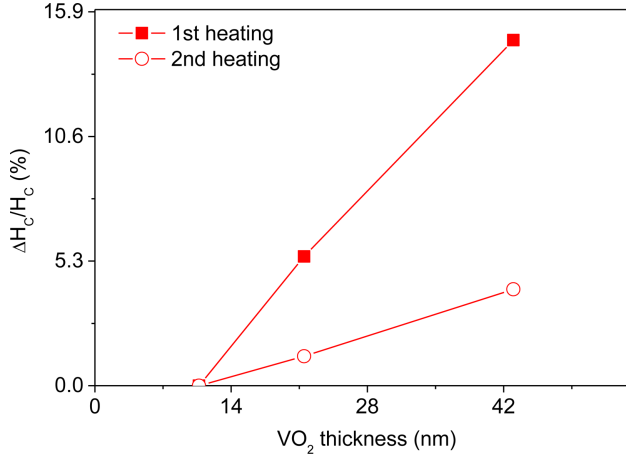
5(c) shows a schematic picture of measurement configuration. For the first heating, the  $H_C(T)$  of the Co film on the 43-nm-thick (101) VO<sub>2</sub> displayed a sudden increase of about 10 Oe at  $T_{MI}$ . Similarly, the sample with the 22-nm-thick (101) VO<sub>2</sub> exhibited a small increment in the  $H_C$



**Fig. 5.** (Color online) Temperature versus hard-axis coercive field  $H_C$  of Co film deposited on (a) 43-nm-, (b) 22-nm-, and (c) 11-nm-thick (101) VO<sub>2</sub>/R-plane Al<sub>2</sub>O<sub>3</sub>. The temperature dependence of the resistance  $R(T)$  of the (101) VO<sub>2</sub> on the R-plane Al<sub>2</sub>O<sub>3</sub> upon heating and cooling is displayed together.

value at  $T_{MI}$ , while the sample with the 11-nm-thick (101) VO<sub>2</sub> did not show an increase at  $T_{MI}$ . For the hard-axis direction, the change in the  $H_C$  value at  $T_{MI}$  also decreased in the cooling procedure after heating.

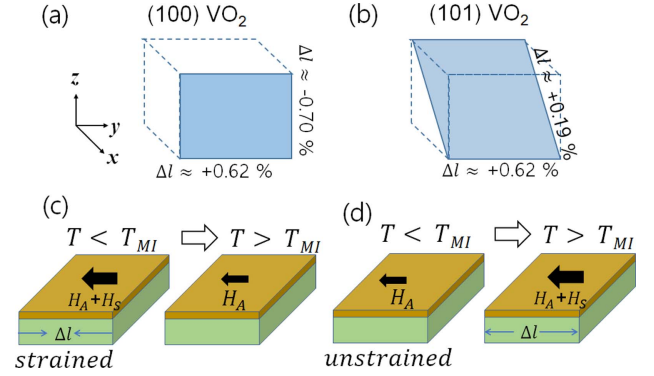
Figure 6 shows the relative change in the coercive field,



**Fig. 6.** (Color online) (101) VO<sub>2</sub> thickness versus relative change in coercive field,  $\Delta H_C/H_C$ , of Co layer along easy axis.

$\Delta H_C/H_C$ , at  $T_{MI}$  with the VO<sub>2</sub> thickness. As the VO<sub>2</sub> thickness increased, the  $\Delta H_C/H_C$  at  $T_{MI}$  displayed a linearly increasing tendency. A certain critical thickness was apparent around  $\sim 11$  nm for the change in the coercive field at  $T_{MI}$ , implying that the magnetoelastic effect can only be observed if the VO<sub>2</sub> thickness is larger than this critical thickness. Previously, Yang *et al.* reported that a 60-nm-thick VO<sub>2</sub> film exhibited a sudden change in the lattice constant  $c$  with a structural phase transition from monoclinic to tetragonal, whereas a 13-nm-thick film did not show any indication of the structural phase transition at  $T_{MI}$  [19]. The absence of a structural phase transition in the thin VO<sub>2</sub> film was explained by an epitaxial stabilization of the tetragonal phase and an epitaxial strain. Therefore, we believe that the observed  $\Delta H_C/H_C$  at  $T_{MI}$  with the VO<sub>2</sub> thickness is consistent with such previous results, and the temperature dependence of the coercive field in the Co layer is dependent on the structural phase transition property of the underlying VO<sub>2</sub> layer.

In the Co/VO<sub>2</sub> sample, the source of strain in the Co layer is the structural phase transition of the underlying VO<sub>2</sub> layer from a monoclinic to a rutile structure. As observed in Figs. 7(a) and (b), we estimated that the structural phase transition of the (100) VO<sub>2</sub> on the C-plane Al<sub>2</sub>O<sub>3</sub> had approximate lattice parameter changes of +0.62 % and –0.7 % for the two in-plane orthogonal directions, whereas such transition of the (101) VO<sub>2</sub> on the R-plane Al<sub>2</sub>O<sub>3</sub> had lattice parameter changes of +0.62 % and +0.19 %. Studies have shown that (100)-oriented rutile oxide films, such as TiO<sub>2</sub>, VO<sub>2</sub>, and CrO<sub>2</sub>, could be heteroepitaxially grown on hexagonal C-plane Al<sub>2</sub>O<sub>3</sub>; however, they will have an in-plane texture because of the existence of three equivalent growth directions within the plane [24]. Therefore, we conjecture that the structural



**Fig. 7.** (Color online) In-plane length change  $\Delta l$  of (a) (100) VO<sub>2</sub> on C-plane Al<sub>2</sub>O<sub>3</sub> and (b) (101) VO<sub>2</sub> on R-plane Al<sub>2</sub>O<sub>3</sub> caused by structural phase transition at  $T_{MI}$ . The in-plane length changes were estimated from the lattice parameters below and above  $T_{MI}$ . Schematic images for anisotropy field changes (c) from strained state to unstrained state and (d) from unstrained state to strained state.  $H_K$  and  $H_A$  represent a stress anisotropy field and a pre-existing anisotropy field, respectively.

phase transition of the underlying (100) VO<sub>2</sub> layer does not effectively generate lattice strain to the neighboring Co layer because two in-plane strains at the unit-cell scale are similar values with opposite signs. That is to say, we think that overall strain effect by small disordered (100) VO<sub>2</sub> grains within the plane is probably negligible because two opposite strain effect will be canceled out each other in a large scale. Presumably lots of small textured (100) VO<sub>2</sub> grains in the plane can't generate a homogeneous strain to the neighboring magnetic film as the single crystal-like (101) VO<sub>2</sub> film even in the plane. We hypothesize that the structural phase transition of the underlying (101) VO<sub>2</sub> on the R-plane Al<sub>2</sub>O<sub>3</sub> can exert a strain effect on the neighboring Co layer through net in-plane strains at the unit-cell scale.

The lattice distortion in the underlying VO<sub>2</sub> layer generates an anisotropic stress on the neighboring Co layer. For the Co/(101)VO<sub>2</sub> on the R-plane Al<sub>2</sub>O<sub>3</sub> sample in Fig. 4(a), the easy-axis coercivity increased from  $\sim 45$  Oe at 325 K to  $\sim 52$  Oe at 345 K. In addition, the hard-axis coercivity in Fig. 5(a) increased from  $\sim 20$  Oe at 325 K to  $\sim 30$  Oe at 345 K. We assume that the coercive field increment of +7 to +10 Oe between 325 and 345 K was due to the stress anisotropy field, which was caused by the structural phase transition of the VO<sub>2</sub> layer. A stress anisotropy effect can be added to other pre-existing anisotropy fields ( $H_A$ ). The stress anisotropy field ( $H_K$ ) is given by the expression [25]

$$H_K = \frac{3\lambda\sigma}{M_S}, \quad (1)$$

where  $\sigma$  is the stress in Pa,  $\lambda$  is the magnetostriction coefficient, and the saturation magnetization  $M_S$  is about 1400 emu/cm<sup>3</sup> (or  $1400 \times 10^3$  A/m) for Co [26]. A net stress of  $-6.6$  to  $-9.4$  MPa would be required at 325 K to produce the  $+7$  to  $+10$  Oe (or  $7 \times 10^{-4}$  to  $10^{-3}$  N/Am) anisotropy field for the Co/(101) VO<sub>2</sub> on the R-plane Al<sub>2</sub>O<sub>3</sub> sample. This negative stress value is distinctively different from the positive stress of  $+22$  MPa in the Ni/(100)VO<sub>2</sub> on the C-plane Al<sub>2</sub>O<sub>3</sub> reported by Lauzier [20]. The magnetostriction coefficients for Co and Ni were reported to be about  $-50 \times 10^{-6}$  and  $-34 \times 10^{-6}$ , respectively [27]. Although both coefficients are negative, the effective stress can be an opposite type because of a difference in the pre-owned strain existing in the magnetic layer. In Lauzier's report, the Ni layer was deposited on VO<sub>2</sub> above  $T_{MI}$ ; hence, it was in a contracted state below  $T_{MI}$  and in an unstrained state above  $T_{MI}$ , as shown in Fig. 7(c). In contrast, our Co film was deposited on VO<sub>2</sub> at room temperature; hence, it was in an unstrained state below  $T_{MI}$  and in an expanded state above  $T_{MI}$ , as shown in Fig. 7(d). A difference in the room temperature state may cause a variation in the pre-owned strain and the strain change with the temperature change across  $T_{MI}$ . Finally, we conjecture that the observed irreversible change of  $H_C$  upon heating and cooling treatments may be due to an imperfect adhesion with the deposition of the metallic Co on the oxide VO<sub>2</sub> at room temperature. An irreversible interfacial change can be induced when the measurement temperature becomes higher than the deposition temperature. Previously, Lauzier had reported that the irreversible change was very small when Ni films was deposited on VO<sub>2</sub> at 473 K [28].

#### 4. Conclusions

In this study, 2.5-nm-thick Co films were deposited on (100) and (101) VO<sub>2</sub> films with thicknesses of 11-43 nm. The VO<sub>2</sub> films were used to induce magnetoelastic coupling with the Co layer because its structural phase transition from monoclinic to tetragonal has a phase-transition-induced strain of  $\sim 0.7$  %. MOKE hysteresis loops were measured with a temperature change of up to 380 K. Upon heating, the coercive field of the Co layer displayed a sudden increase at  $\sim T_{MI}$ , indicating a significant magnetoelastic coupling between the Co and VO<sub>2</sub> layers. However, this increment diminished with decreasing VO<sub>2</sub> thickness, and it disappeared as the VO<sub>2</sub> became thinner than a critical value of  $\sim 11$  nm. Our results suggest that a phase-transition-induced strain in the VO<sub>2</sub> layer can be used to modify the coercive field in the neighboring magnetic layer.

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