

Amorphous Cr-Ti Texture-inducing Layer Underlying (002) Textured bcc-Cr alloy Seed Layer for FePt-C Based Heat-assisted Magnetic Recording Media

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$\text{Cr}_{100-x}\text{Ti}_x$ amorphous texture-inducing layers (TIL) were investigated to realize highly (002) oriented L1_0 FePt-C granular films through hetero-epitaxial growth on the (002) textured bcc- $\text{Cr}_{80}\text{Mn}_{20}$ seed layer (bcc-SL). As-deposited TILs showed the amorphous phase in Ti content of $30 \leq x \text{ (at\%)} \leq 75$. Particularly, films with $40 \leq x \leq 60$ kept the amorphous phase against the heat treatment over 600 °C. It was found that preference of the crystallographic texture for bcc-SLs is directly affected by the structural phase of TILs. (002) crystallographic texture was realized in bcc-SLs deposited on the amorphous TILs ($40 \leq x \leq 70$), whereas (110) texture was formed in bcc-SLs overlying on crystalline TILs ($x < 30$ and $x > 70$). Correlation between the angular distribution of (002) crystal orientation of bcc-SL evaluated by full width at half maximum of (002) diffraction (FWHM) and a grain diameter of bcc-SL indicated that while the development of the lateral growth for bcc-SL grain reduces FWHM, crystallization of amorphous TILs hinders FWHM. L1_0 FePt-C granular films were fabricated under the substrate heating process over 600 °C with having different FWHM of bcc-SL. Hysteresis loops showed that squareness (M_r/M_s) of the films increased from 0.87 to 0.95 when FWHM of bcc-SL decreased from 13.7 ° to 3.8 °. It is suggested that the reduction of (002) FWHM affects to the overlying MgO film as well as FePt-C granular film by means of the hetero-epitaxial growth.

Keywords : amorphous Cr-Ti texture inducing layer, bcc-Cr alloy seed layer, lateral grain growth, hetero-epitaxial growth, L1_0 FePt-C granular film, angular distribution of c -axis

1. Introduction

The hard disk drive (HDD) industry has been gradually developed over several decades by increasing the areal density (AD). While current HDD based on CoPtCr-oxide granular film is expected to limit the maximum AD of 1.0-1.5 Tb/in², heat-assisted magnetic recording (HAMR) media based on L1_0 FePt granular film is considered to extend the maximum AD over 4 Tb/in² owing to the high magnetocrystalline anisotropy of L1_0 ordered phase for FePt ($K_u \sim 7 \times 10^7 \text{ erg/cm}^3$) [1-3]. In order to realize the L1_0 ordered FePt granular film as a high recording density medium, it is necessary to enhance the signal-to-noise ratio (SNR). Contribution to the SNR can result from variation in the angular distribution of c -axis orientation of L1_0 FePt grains. Since the c -axis orientation,

which corresponds to the easy magnetized axis for the L1_0 ordered FePt, can be adjusted by hetero-epitaxial growth from (002) textured crystalline seed layer (SL), the angular distribution of the c -axis is mainly attributed to that of SL. Recently, we reported the concept to suppress the angular distribution of the (002) orientation of SL [4]. The origin of the angular distribution of the crystal orientation can be described by considering the formation of crystalline facets during the solidification of the liquid phase of sputtered atoms under the different wettability of SL on an amorphous texture-inducing layer (a -TIL). Low wettability condition induces the ball-shaped liquid phase of the sputtered atoms, whereas high wettability condition tends to spread the liquid phase over the surface of a -TIL. During the solidification, the liquid phase changes to the crystalline facet in order to form the crystallographic texture. In the case of the low wettability, the crystalline facets have much more chance to form the crystalline plane with various angles from normal to the film plane. Consequently, the crystallographic texture can

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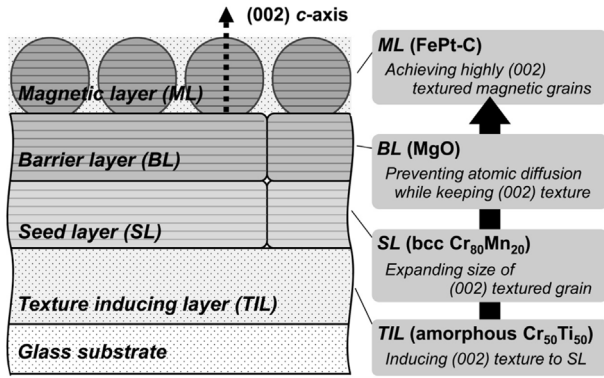


Fig. 1. Schematic representation to suppress angular distribution of (002) *c*-axis orientation for FePt-C granular film.

be slanted from normal to the film plane. In the case of the high wettability, the most surface of the crystalline facets is parallel to the normal to the plane, which induces the development of the crystallographic texture without a tilt of the crystal orientation. Providing that the solidification determines the texture, fabrication of the large grain SL is essential. Based on the concept, a designed stacking structure is illustrated in Fig. 1. We found that the materials combination between bcc-Cr alloy SL and $\text{Cr}_{50}\text{Ti}_{50}$ *a*-TIL promoted the lateral grain growth for bcc-Cr alloy SL. However, crystallization of the $\text{Cr}_{50}\text{Ti}_{50}$ *a*-TIL induced by post-annealing process suppressed the development of the lateral grain growth. In order to increase the grain size of bcc-Cr alloy SL, investigation on the degree of amorphous and thermal stability of amorphous is inevitable. In this research, quantitative study on the amorphous Cr-Ti TILs was carried out for (002) texture formation of bcc-Cr alloy SL.

2. Experimental Procedure

All samples used in this study were fabricated by using in-line magnetron sputtering system (Canon Anelva C-3010). The stacking structure of the samples was composed of $\text{Cr}_{80}\text{Mn}_{20}$ (30 nm)/ $\text{Cr}_{100-x}\text{Ti}_x$ (20 nm)/ $\text{Ni}_{60}\text{Ta}_{40}$ (2 nm)/nanocrystalline glass substrate. Here, $\text{Ni}_{60}\text{Ta}_{40}$ was introduced to promote the amorphous structure for $\text{Cr}_{100-x}\text{Ti}_x$ TIL. $\text{Cr}_{100-x}\text{Ti}_x$ TIL was deposited by co-sputtering Cr and Ti under 0.6 Pa Ar with a deposition rate of 0.5 nm/sec. Ti content was varied from 0 to 100 at%, and then $\text{Cr}_{80}\text{Mn}_{20}$ was deposited on $\text{Cr}_{100-x}\text{Ti}_x$ TIL under 0.8 Pa Ar with a deposition rate of 3.2 nm/sec. The substrate temperature could be elevated from RT to 600 °C before deposition of bcc- $\text{Cr}_{80}\text{Mn}_{20}$ SL (Hereafter, bcc-SL) to induce the lateral growth of bcc-SL grains without the atomic diffusion due to the phase stability of the alloy

system [5]. The base pressure of all chambers was kept approximately 5×10^{-6} Pa. Structure analysis was carried out by X-ray diffractometry (XRD). The grain size of bcc-SL was derived by using Scherrer's equation with a full width at half maximum (FWHM) at a Bragg angle for CrMn (200) diffraction obtained from in-plane XRD [6]. The angular distribution of (002) crystal orientation of bcc-SL was evaluated by measuring rocking curve at (002) diffraction. Magnetic properties of FePt-C granular films were investigated by a SQUIDS-VSM with an applied magnetic field normal to the film plane up to 65 kOe at room temperature.

3. Result and Discussion

3.1. Amorphous formation and its thermal stability of $\text{Cr}_{100-x}\text{Ti}_x$ TILs

Figure 2 shows in-plane XRD patterns of (a) as-deposited and (b) post-annealed up to a temperature of 600 °C for $\text{Cr}_{100-x}\text{Ti}_x$ (20 nm) TILs on NiTa (2 nm)/glass substrate with various Ti content. In the case of (a) as-deposited state, two diffractions at Bragg angles of $2\theta_\chi = 44^\circ$ and 64° were observed in $x = 0$ (pure bcc-Cr) TIL. These diffractions, which were identified (110) and (220) diffractions of bcc-Cr powder, gradually shifted to lower angles with the increase of $x = 0$ to 20 at%. The result indicates that the atomic substitution from Cr to Ti induces the increase of the lattice volume while sustaining the crystalline structure. However, change of the diffraction width from the narrow to broad signal was observed with the further increase of x from 20 to 30 at%, and then the broad signal was obtained regardless of the increase of x

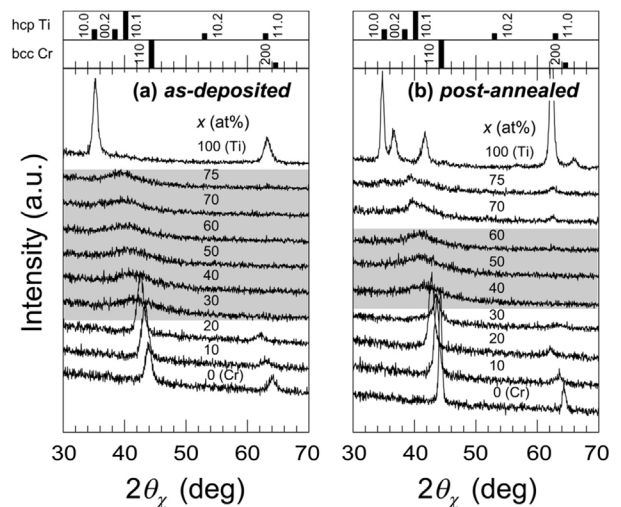


Fig. 2. In-plane XRD patterns of (a) as-deposited and (b) post-annealed $\text{Cr}_{100-x}\text{Ti}_x$ (20 nm) TILs on NiTa (2 nm)/glass substrate with various Ti content (x).

up to 75 at%. This result suggests that the amount of the constructive interference of X-rays decreased due to the randomly located atoms (i.e. amorphous phase). Again, two diffractions at Bragg angles of $2\theta_\chi = 35^\circ$ and 63° were obtained in $x = 100$ (pure hcp-Ti) TIL. In the case of (b) post-annealed TILs, one can see that additional diffractions occurred at $2\theta_\chi = 40\text{--}44^\circ$ and 64° in $x = 30, 70,$ and 75 at% as compared with the as-deposited TILs. The result suggests that these films experienced the crystallization. Only the films with x from 40 to 60 at% maintained the amorphous phase against the heat treatment.

3.2. Preferred crystal orientation and its angular distribution of bcc-SL on $\text{Cr}_{100-x}\text{Ti}_x$ TILs

Figure 3 shows out-of-plane XRD patterns of bcc-SL on $\text{Cr}_{100-x}\text{Ti}_x(20\text{ nm})/\text{NiTa}(2\text{ nm})/\text{glass}$ substrate with various x (a) without and (b) with the substrate heating process. In the case of (a) bcc-SL without substrate heating process, a continuous change in preference of the crystallographic texture was observed with the increase of x . Distinct diffraction at $2\theta \sim 44^\circ$ was observed when bcc-SL was deposited on pure Cr ($x = 0$) TIL. It was confirmed that the (110) sheet texture was formed in bcc-SL by comparing Bragg angle of bcc-SL to that of bcc-Cr powder. The intensity of the (110) diffraction rapidly decreased with the increase of x from 0 to 30 at%, and then the preference of the crystallographic texture was vanished at $x = 40$ at%. However, change in the preferred crystal orientation from (110) to (002) was observed at $x = 50$ and 60 at%. Further increase of x induced (110) sheet texture for bcc-SL. In the case of (b) bcc-SL with the substrate heating process, integrated intensity of all

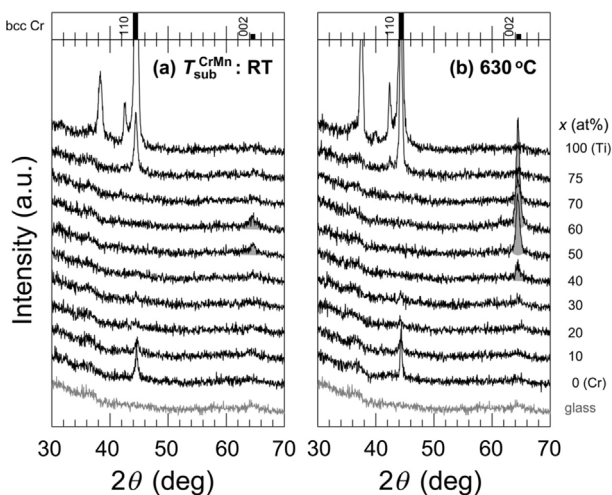


Fig. 3. Out-of-plane XRD patterns of bcc-SL on $\text{Cr}_{100-x}\text{Ti}_x(20\text{ nm})/\text{NiTa}(2\text{ nm})/\text{glass}$ substrate with various Ti content (a) without and (b) with substrate heating process.

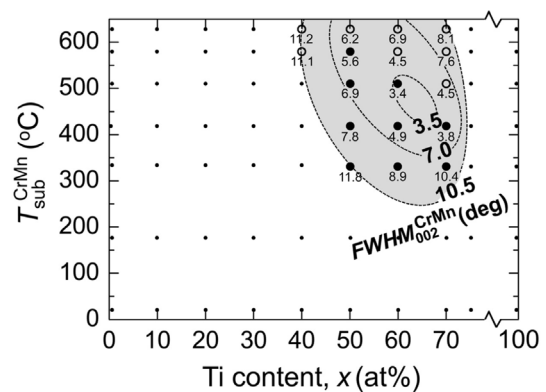


Fig. 4. Angular distribution of (002) crystal orientation (FWHM) of bcc-SL varied with substrate temperature (T_{sub}) and Ti content (x).

diffractions increased. Furthermore, one can see that the extra (002) diffraction appeared at $x = 40$ and 70 . It is suggested that the increased grain size enhanced the amount of constructive interference of X-ray. It is worth noting that (002) texture formation in bcc-SL is closely related to the formation of amorphous phase in $\text{Cr}_{100-x}\text{Ti}_x$ TILs.

Figure 4 shows the angular distribution of (002) crystal orientation of bcc-SL derived from the full width at half maximum (FWHM) varied with T_{sub} and x . Measured range for (002) sheet texture (gray region) is limited by both $T_{\text{sub}} \geq 300^\circ\text{C}$ and $30 < x (\text{at}\%) < 75$. Note that this composition range corresponds to the amorphous formation region for $\text{Cr}_{100-x}\text{Ti}_x$ TILs. In addition, the magnitude of FWHM along the same x decreased with increasing T_{sub} (solid circle ●) and then, decreased with further increasing T_{sub} (open circle ○) within x of 50 to 70 at%.

Figure 5 shows variation in grain diameter (GD) of bcc-SL varied with T_{sub} and x . To evaluate GD, CrMn (200) peak measured by in-plane X-ray diffraction was used

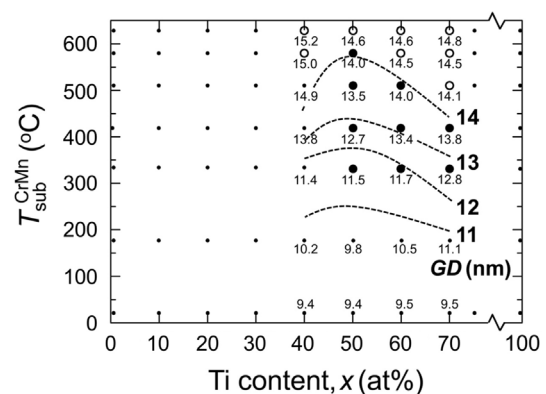


Fig. 5. Variation in grain diameter (GD) of bcc-SL with respect to substrate temperature T_{sub} and Ti content (x).

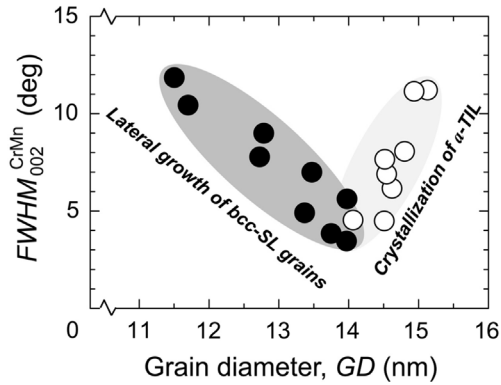


Fig. 6. Correlation between (002) FWHM and GD of bcc-SL.

(not shown in this paper). It is clearly shown that GD gradually increased as the increase of T_{sub} regardless of x . The result indicates that the high substrate temperature enhances the adatomic mobility during solidification that induces lateral grain growth in the film.

Figure 6 represents the correlation between (002) FWHM and GD of bcc-SLs. (002) FWHM decreased from 11.8° to 3.4° as the increase of GD from 11.5 nm to 14.0 nm, and then (002) FWHM increased as further increase of GD. While the development of the lateral growth for bcc-SL grain suppresses (002) FWHM, crystallization of the amorphous Cr-Ti TILs deteriorates the quality of (002) texture. The result suggests that exploring the amorphous materials with the high crystallization temperature is inevitable to realize highly (002) textured SL.

3.3. Magnetic properties of FePt-C granular films with highly (002) textured bcc-SL

FePt-C granular films were prepared to clarify the effect of (002) FWHM of bcc-SL on the magnetic properties of the film. The stacked structure consists of FePt-C/MgO/CrMn/CrTi/glass sub. (002) FWHM of bcc-SL was manipulated by changing the fabrication conditions for CrMn and CrTi whereas the sputtering conditions for MgO and FePt-C was fixed. To promote the $L1_0$ ordered phase for FePt, the substrate temperature was elevated about 600°C before deposition of FePt-C film [7, 8]. Figure 7 shows the out-of-plane magnetization curve for the $L1_0$ FePt-C granular films with (002) FWHM of 3.8 (solid), 4.2 (dash), and 13.7 (dot). All hysteresis loops show the constant magnetization while an applied magnetic field decreases from 65 kOe to 5 kOe, and then the magnetization gradually decreased with the decrease in the magnetic field intensity from 5 kOe to -50 kOe. It is shown that the required field to reverse the magnetization is over 50 kOe. The result indicates that

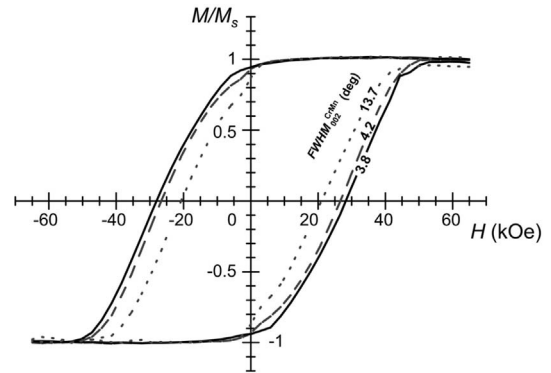


Fig. 7. Out-of-plane M-H loops of FePt-C granular films with bcc-SL (002) FWHM of 3.8° (solid line), 4.2° (dashed line), and 13.7° (dotted line).

the $L1_0$ ordered phase for FePt-C granular films in which the magnetic easy-axis is aligned toward normal to the film plane is realized. It is clear that both the coercivity and squareness (M/M_s) of the films gradually increased as the decrease in (002) FWHM. The quantitative result suggests that the reduction of (002) FWHM of bcc-SL affects to the overlying MgO film as well as FePt-C granular film by means of the hetero-epitaxial growth. Consequently, it is suggested that the reduction of the angular distribution of the magnetized easy axis enhances the perpendicular hysteresis.

4. Conclusion

$\text{Cr}_{100-x}\text{Ti}_x$ amorphous texture-inducing layers (TIL) were investigated to realize highly (002) textured FePt-C granular film through the (002) texture formation of CrMn SL. As-deposited $\text{Cr}_{100-x}\text{Ti}_x$ TILs showed amorphous phase in the range of $30 \leq x$ (at%) ≤ 75 . Particularly, those films with the composition range of $40 \leq x \leq 60$ kept the amorphous phase against the heat treatment over 600°C . It was found that the preference of the crystallographic orientation for CrMn SL is directly affected by structural phase of $\text{Cr}_{100-x}\text{Ti}_x$ TILs. (002) preferred crystal orientation was realized when CrMn is deposited on amorphous $\text{Cr}_{100-x}\text{Ti}_x$ TILs ($40 \leq x \leq 70$). Otherwise, (110) orientation was formed. Correlation between the angular distribution of CrMn (002) crystal orientation (FWHM) and the grain diameter (GD) of CrMn SLs has been examined. While the development of the lateral growth for CrMn grain suppress FWHM, crystallization of Cr-Ti a -TILs hinders the quality of (002) texture. It is suggested that the reduction of the angular distribution of the magnetic easy axis due to the highly (002) textured CrMn SL enhances the perpendicular hysteresis in FePt-C granular film.

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